

The logo for ARTEMIS, featuring the word in a stylized, italicized font with a blue and orange wave-like graphic behind it.The logo for CNRS (Centre National de la Recherche Scientifique), consisting of the letters 'CNRS' in a stylized, blue font.The logo for Observatoire de la Côte d'Azur, featuring the text in a serif font with a small graphic of three stars above it.

unusual LISA

Jean-Yves Vinet
A.R.T.E.M.I.S.
Observatoire de la Côte d'Azur
NICE (France)

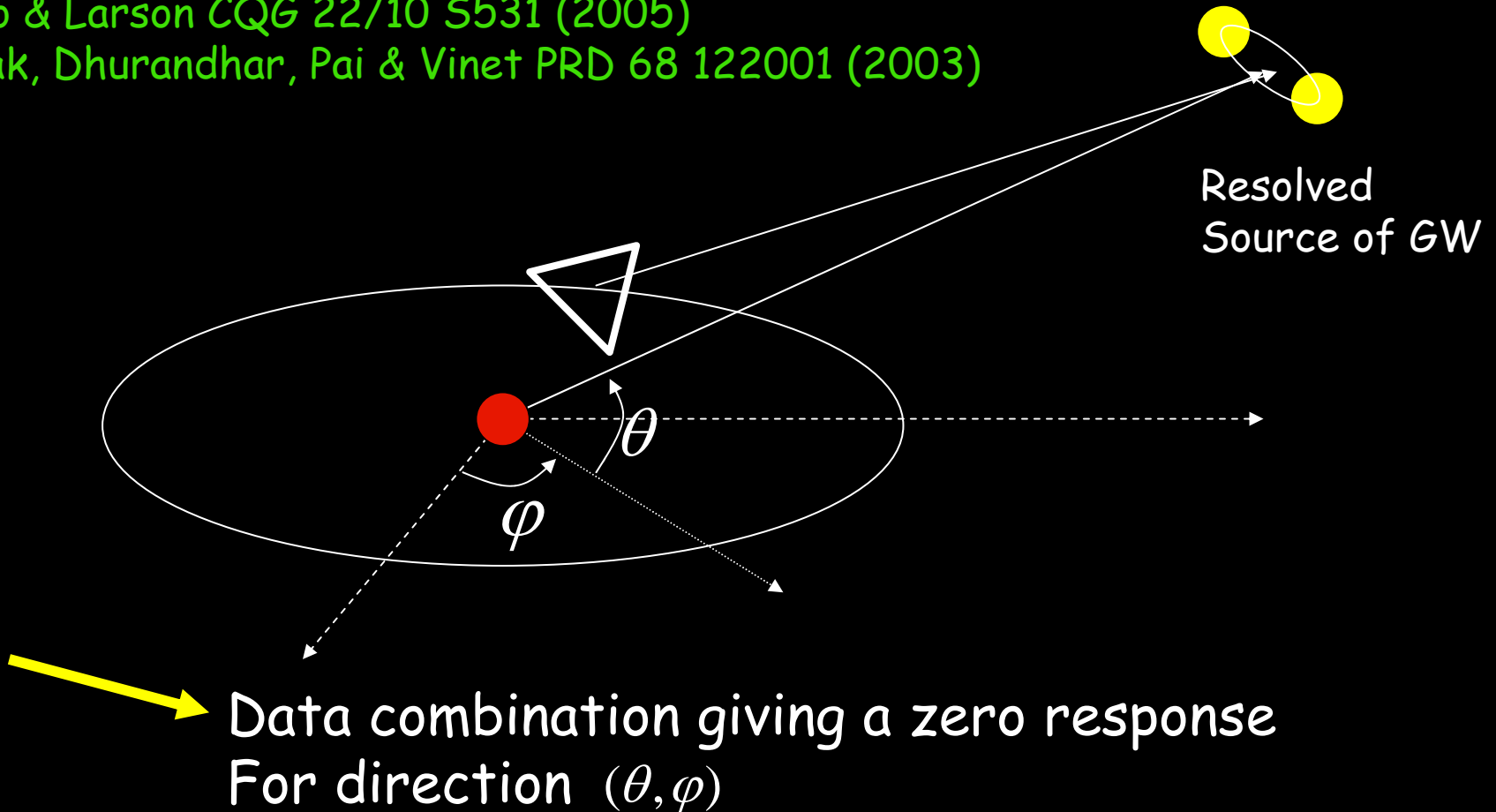
Contents

- 1) Gravitational coronagraphy
- 2) Signals from asteroids

Gravitational coronagraphy

Tinto & Larson *CQG* 22/10 S531 (2005)

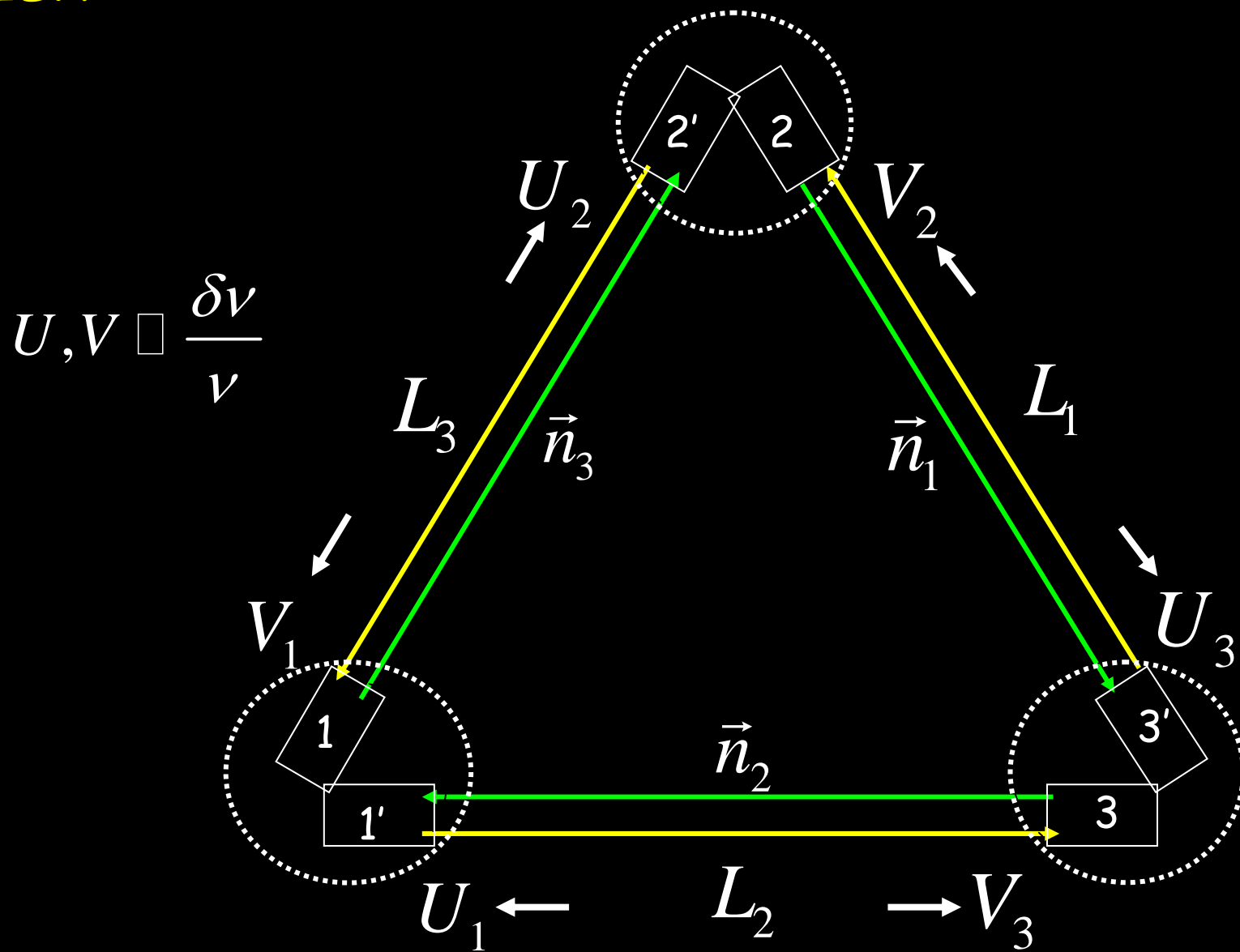
Nayak, Dhurandhar, Pai & Vinet *PRD* 68 122001 (2003)



Benefits (conjecture)

- Occultation of a strong source for better analysis of its angular neighborhood
- Improving angular resolution

LISA



Recall

- 6 main data channels (1 per phasemeter)
- There exist families of combinations of the 6 flows with properly chosen time delays that cancel dominant instrumental noises → TDI (Time Delay Interferometry)
(Tinto, Armstrong, Estabrook, 99)
- They form a module and have generating parts (sets of generators).
(Dhurandhar, Nayak, Vinet, 02)
- One may combine these generators for special purposes, keeping the noise cancelling property

Recall

- The generators have the form:

$$g = (p_1, p_2, p_3, q_1, q_2, q_3)$$

- Where (p_i, q_i) are formal polynomials in the 3 delay operators D_a

$$(D_a f)(t) \equiv f(t - L_a) \quad (a = 1, 2, 3)$$

Recall

6-uple of data:

$$\mathbf{U}(t) = [V_1(t), V_2(t), V_3(t), U_1(t), U_2(t), U_3(t)]$$

Generic noise-cancelling combination g :

$$\langle g | \mathbf{U} \rangle (t) = \sum_{i=1}^3 [p_i V(t)_i + q_i U_i(t)]$$

= 0 when U, V represent laser phase fluctuations

Notation

Source oriented unit vector : $\vec{w}(\theta, \varphi)$

3 orthonormal vectors : $\vec{w}, \vec{\theta} = \frac{\partial \vec{w}}{\partial \theta}, \vec{\varphi} = \frac{1}{\sin \theta} \frac{\partial \vec{w}}{\partial \varphi}$

Unit vector along arm #a : \vec{n}_a ($a = 1, 2, 3$)

Directional functions (spin 2 harmonics):

$$\xi_{a+} = (\vec{\theta} \cdot \vec{n}_a)^2 - (\vec{\varphi} \cdot \vec{n}_a)^2$$

$$\xi_{a\times} = 2(\vec{\theta} \cdot \vec{n}_a)(\vec{\varphi} \cdot \vec{n}_a)$$

Location of node #a : \vec{r}_a notation $\mu_a = \vec{w} \cdot \vec{r}_a$

Notation

h_+, h_x : the 2 polarization components of the GW

Data flow at node # 1 :

$$U_{1+,x}(t) = -\frac{h_{+,x}(t - \mu_1) - h_{+,x}(t - \mu_3 - L_2)}{2(1 + \vec{w} \cdot \vec{n}_2)} \xi_{2+,x}$$

$$V_{1+,x}(t) = \frac{h_{+,x}(t - \mu_1) - h_{+,x}(t - \mu_2 - L_3)}{2(1 - \vec{w} \cdot \vec{n}_3)} \xi_{3+,x}$$

Others are obtained by circular permutation of indices

Notation

Fourier space : transfer functions:

$$U_a = F_{U_a+} \tilde{h}_+ + F_{U_a\times} \tilde{h}_\times \quad , \quad V_a = F_{V_a+} \tilde{h}_+ + F_{V_a\times} \tilde{h}_\times$$

$$F_{V_{1+,\times}} = \frac{e^{i\omega\mu_1} - e^{i\omega(\mu_2+L_3)}}{2(1 - \vec{w} \cdot \vec{n}_3)} \xi_{3+,\times} \quad , \quad F_{U_{1+,\times}} = -\frac{e^{i\omega\mu_1} - e^{i\omega(\mu_3+L_2)}}{2(1 + \vec{w} \cdot \vec{n}_2)} \xi_{2+,\times}$$

+ circular permutations

6-uple transfer:

$$\mathbf{F}_{+,\times} = (F_{V_{1+,\times}}, F_{V_{2+,\times}}, F_{V_{3+,\times}}, F_{U_{1+,\times}}, F_{U_{2+,\times}}, F_{U_{3+,\times}})$$

Notation

- Example of generators (Tinto et al.)

$$\alpha = (1, D_3, D_1 D_3, 1, D_1 D_2, D_2)$$

$$\beta = (D_1 D_2, 1, D_1, D_3, 1, D_2 D_3)$$

$$\gamma = (D_2, D_2 D_3, 1, D_1 D_3, D_1, 1)$$

and ζ

- Vector generator: $\vec{Y} = \begin{bmatrix} \alpha \\ \beta \\ \gamma \end{bmatrix}$

Algebraic solution

Generic combination C :

$$C = C_1\alpha + C_2\beta + C_3\gamma = \vec{C} \cdot \vec{Y}$$

Transfer function:

$$\begin{aligned} \tilde{h}_C(f) &= \langle C | F_+ \rangle \tilde{h}_+(f) + \langle C | F_x \rangle \tilde{h}(f)_x = \\ & \vec{C} \cdot \langle \vec{Y} | F_+ \rangle \tilde{h}_+(f) + \vec{C} \cdot \langle \vec{Y} | F_x \rangle \tilde{h}_x(f) \end{aligned}$$

Algebraic formal solution

For cancelling any signal, we must have simultaneously:

$$\vec{C} \cdot \langle \vec{Y} | \mathbf{F}_+ \rangle = 0, \quad \vec{C} \cdot \langle \vec{Y} | \mathbf{F}_\times \rangle = 0$$

Thus:

$$\vec{C} = \langle \vec{Y} | \mathbf{F}_+ \rangle \times \langle \vec{Y} | \mathbf{F}_\times \rangle$$

Explicit solution

1) The transfer functions $F_{\alpha+,x} = \langle \alpha | F_{+,x} \rangle$

May be considered as scalar products with
The directional functions ξ :

$$\vec{\xi}_{+,x} = (\xi_{+,x1}, \xi_{2+,x}, \xi_{3+,x})$$

then $\exists \vec{\alpha}, \vec{\beta}, \vec{\gamma} : F_{\alpha,\beta,\gamma+,x} = (\vec{\alpha}, \vec{\beta}, \vec{\gamma}) \cdot \vec{\xi}_{+,x}$

And

$$\vec{C} = \begin{bmatrix} (\vec{\beta} \times \vec{\gamma}) \cdot (\vec{\xi}_+ \times \vec{\xi}_x) \\ (\vec{\gamma} \times \vec{\alpha}) \cdot (\vec{\xi}_+ \times \vec{\xi}_x) \\ (\vec{\alpha} \times \vec{\beta}) \cdot (\vec{\xi}_+ \times \vec{\xi}_x) \end{bmatrix}_{15}$$

Explicit solution

Recall:

$$F_{V_{1+,x}} = \frac{e^{i\omega\mu_1} - e^{i\omega(\mu_2+L_3)}}{2(1 - \vec{w} \cdot \vec{n}_3)} \xi_{3+,x}, \quad F_{U_{1+,x}} = -\frac{e^{i\omega\mu_1} - e^{i\omega(\mu_3+L_2)}}{2(1 + \vec{w} \cdot \vec{n}_2)} \xi_{2+,x}$$

Notation: $g_a = e^{i\omega\mu_a}, \quad e_a = e^{i\omega L_a}$

$$v_a = 1 - \vec{n}_a \cdot \vec{w}, \quad u_a = 1 + \vec{n}_a \cdot \vec{w}$$

$$G_3 = \frac{g_1 - g_2 e_3}{v_3}, \quad H_2 = \frac{g_1 - g_3 e_2}{u_2}$$

Explicit Solution

then:

$$\vec{\alpha} = \frac{1}{2} \begin{bmatrix} e_3 G_1 - e_2 H_1 \\ e_1 e_3 G_2 - H_2 \\ G_3 - e_1 e_2 H_3 \end{bmatrix}, \vec{\beta} = \frac{1}{2} \begin{bmatrix} G_1 - e_2 e_3 H_1 \\ e_1 G_2 - e_3 H_2 \\ e_1 e_2 G_3 - H_3 \end{bmatrix}, \vec{\gamma} = \frac{1}{2} \begin{bmatrix} e_2 e_3 G_1 - H_1 \\ G_2 - e_1 e_3 H_2 \\ e_2 G_3 - e_1 H_3 \end{bmatrix}$$

Invariance under simultaneous circular permutation of:

- Vectors
- Components
- Indices

Explicit Solution

The direction \vec{w}_B of the source is constant
In the barycentric frame

There exists a linear mapping to the LISA frame :

$$\vec{w}(t_o) = \mathbf{R}(t_o) \cdot \vec{w}_B$$

Orbital time parameter, very slowly varying with respect to
The « signal time »

Explicit Solution

All functions may be expressed in terms of \vec{w}

$$\left\{ \begin{array}{l} (u, v)_1 = 1 \mp w_2, \quad \mu_1 = Lw_1 / \sqrt{3} \\ (u, v)_2 = 1 \pm \frac{1}{2}(w_2 - \sqrt{3}w_1), \quad \mu_2 = -L(w_1 + \sqrt{3}w_2) / 2\sqrt{3} \\ (u, v)_3 = 1 \pm \frac{1}{2}(w_2 + \sqrt{3}w_1), \quad \mu_3 = -L(w_1 - \sqrt{3}w_2) / 2\sqrt{3} \end{array} \right.$$

$$\vec{\eta} \equiv \vec{\xi}_+ \times \vec{\xi}_\times = \frac{\sqrt{3}}{4} w_3 \begin{bmatrix} 1 + w_3^2 - 2w_1^2 + 2w_2^2 \\ 1 + w_3^2 + w_1^2 - w_2^2 - 2\sqrt{3}w_1w_2 \\ 1 + w_3^2 + w_1^2 - w_2^2 + 2\sqrt{3}w_1w_2 \end{bmatrix}$$

Explicit Solution

$$\begin{aligned}
 C_1 = & \frac{\eta_1}{4u_2v_2u_3v_3} (1 - e_1^2) \left[u_2v_3(\bar{g}_1 - e_3\bar{g}_2 - e_2\bar{g}_3 + e_2e_3g_1^2) - u_3v_2e_2e_3(g_1^2 - e_2\bar{g}_2 - e_3\bar{g}_3 + e_2e_3\bar{g}_1) \right] \\
 & + \frac{\eta_2}{4u_1v_1u_3v_3} \left\{ (1 - e_1e_2e_3) \left[v_1v_3(\bar{g}_1 - e_3\bar{g}_2 - e_1g_2^2 + e_1e_3\bar{g}_3) \right. \right. \\
 & \quad \left. \left. - u_1u_3e_2(\bar{g}_3 - e_1\bar{g}_2 - e_3g_2^2 + e_1e_3\bar{g}_1) \right] \right. \\
 & \quad \left. + (e_1 - e_2e_3) \left[u_1v_3(g_2^2 - e_3\bar{g}_3 - e_1\bar{g}_1 + e_1e_3\bar{g}_2) \right. \right. \\
 & \quad \left. \left. - u_3v_1e_2(\bar{g}_2 - e_1\bar{g}_3 - e_3\bar{g}_1 + e_1e_3g_2^2) \right] \right\} \\
 & + \frac{\eta_3}{4u_1v_1u_2v_2} \left\{ (1 - e_1e_2e_3) \left[u_1u_2(\bar{g}_1 - e_3\bar{g}_3 - e_1g_3^2 + e_1e_2\bar{g}_2) \right. \right. \\
 & \quad \left. \left. - v_1v_2e_3(\bar{g}_2 - e_1\bar{g}_3 - e_2g_3^2 + e_1e_2\bar{g}_1) \right] \right. \\
 & \quad \left. + (e_1 - e_2e_3) \left[v_1u_2(g_3^2 - e_2\bar{g}_2 - e_1\bar{g}_1 + e_1e_2\bar{g}_3) \right. \right. \\
 & \quad \left. \left. - u_1v_2e_2(\bar{g}_3 - e_2\bar{g}_1 - e_1\bar{g}_2 + e_1e_2g_3^2) \right] \right\}
 \end{aligned}$$

33 different delays

Explicit Solution

For retrieving the time domain, simply replace the Phase factors

$$e_a = e^{i\omega L_a}, \quad g_a = e^{i\omega \mu_a}$$

By delay operators

$$(D_a f)(t) = f(t - L_a), \quad (\Gamma_a f)(t) = f(t - \mu_a)$$

the delays L_a et μ_a are slowly varying

L_a Due to the orbital deformation of the triangle (flexing)

μ_a Due to the apparent motion of the source viewed from LISA

Implementation

- Generators (α, β, γ) explicit above are valid for A static LISA (1st generation TDI)
- For actually cancel the instrumental noises one must use The 2d generation TDI generators (more complex)
- For studying the gravitational response, the 1st generation is relevant
- For the gravitational response, the 2d generation amounts to an extra delay

Actual Coronagraphic Combination

$$C = C_1(t_o)\alpha^{(2)} + C_2(t_o)\beta^{(2)} + C_3(t_o)\gamma^{(2)}$$

Our coefficients
(found above)

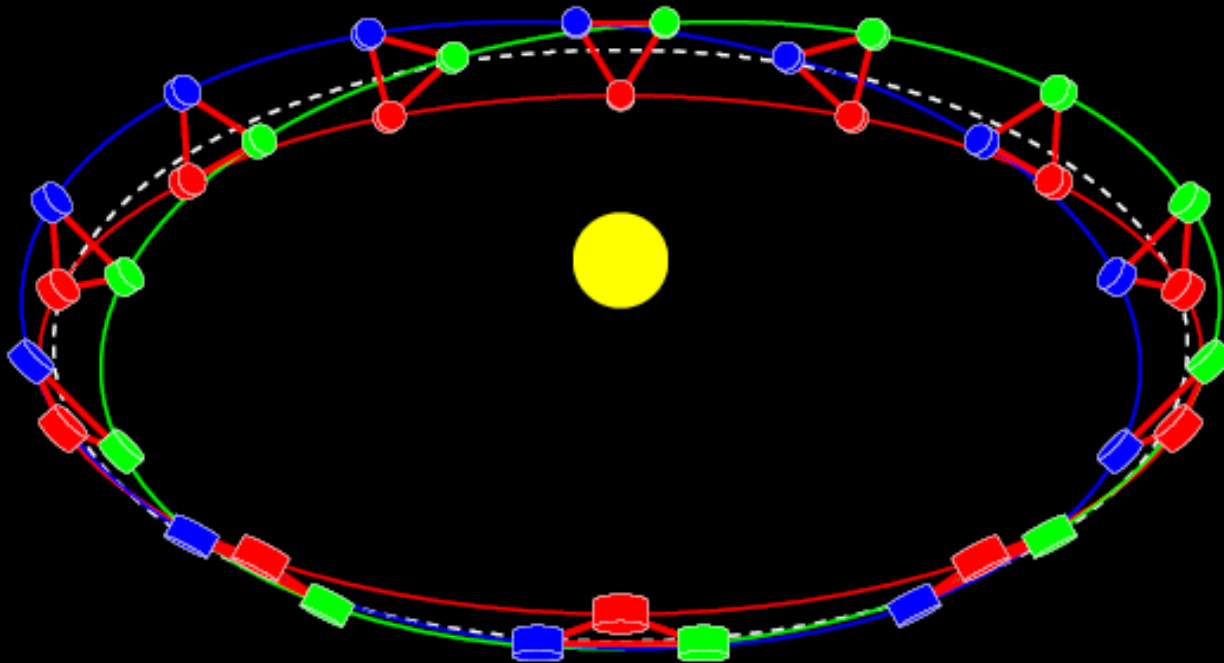
2d generation TDI generators

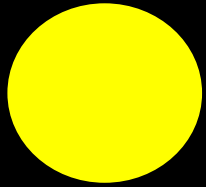
Programme :

Testing the algorithm on mock data

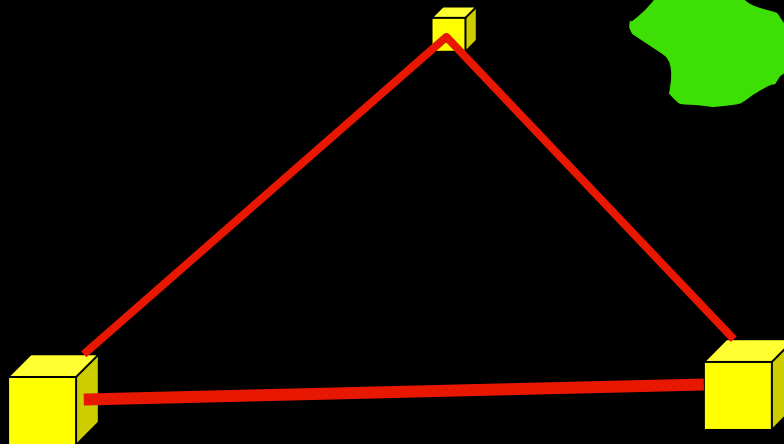
Simulator : **LISACode** (APC-Paris+ARTEMIS-Nice)

http://www.apc.univ-paris7.fr/SPIP/article.php3?id_article=164





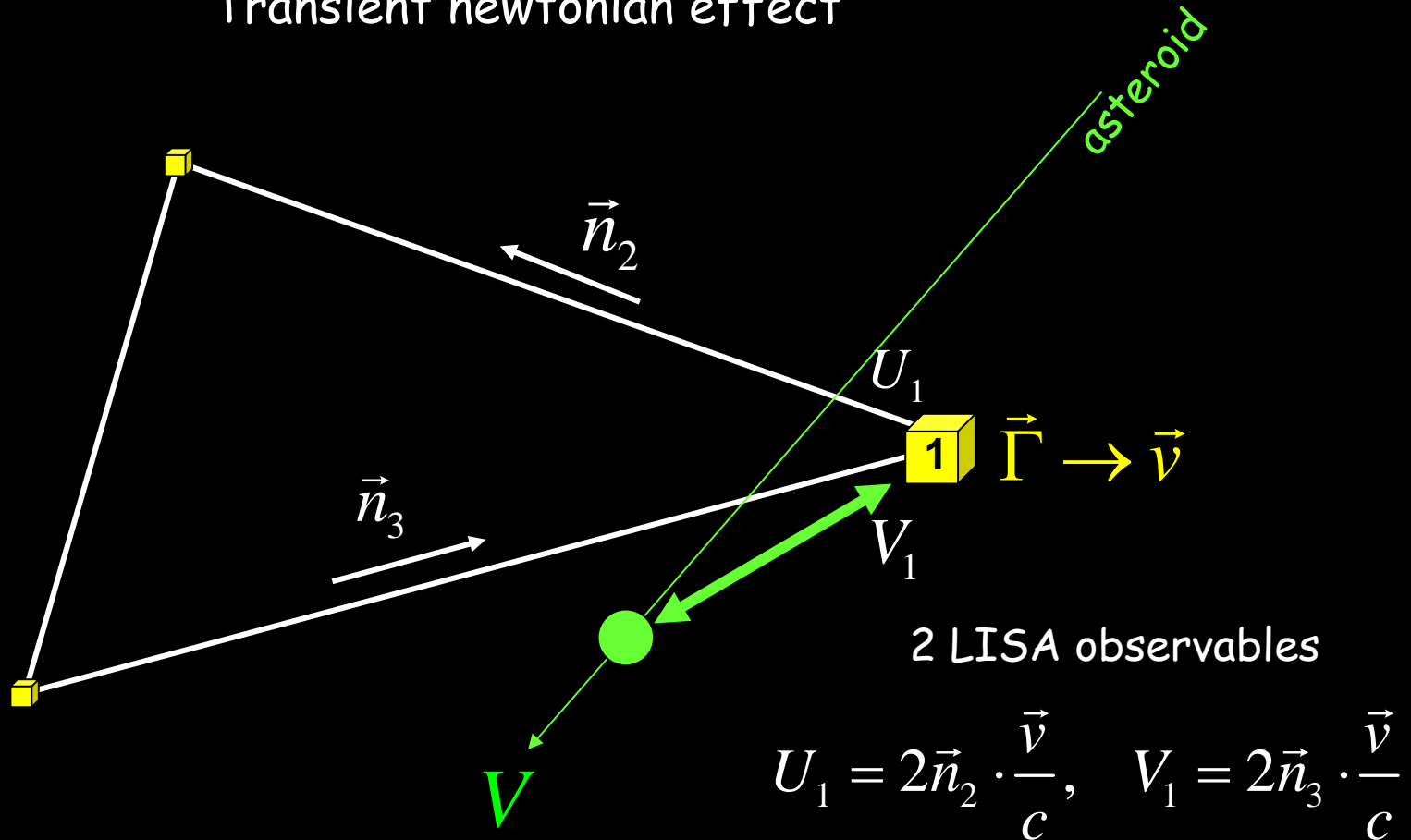
LISA and Asteroids



Vinet, *Class. and Quantum Grav.* 23 (2006) 4939-4944

An asteroid encounter

Transient newtonian effect

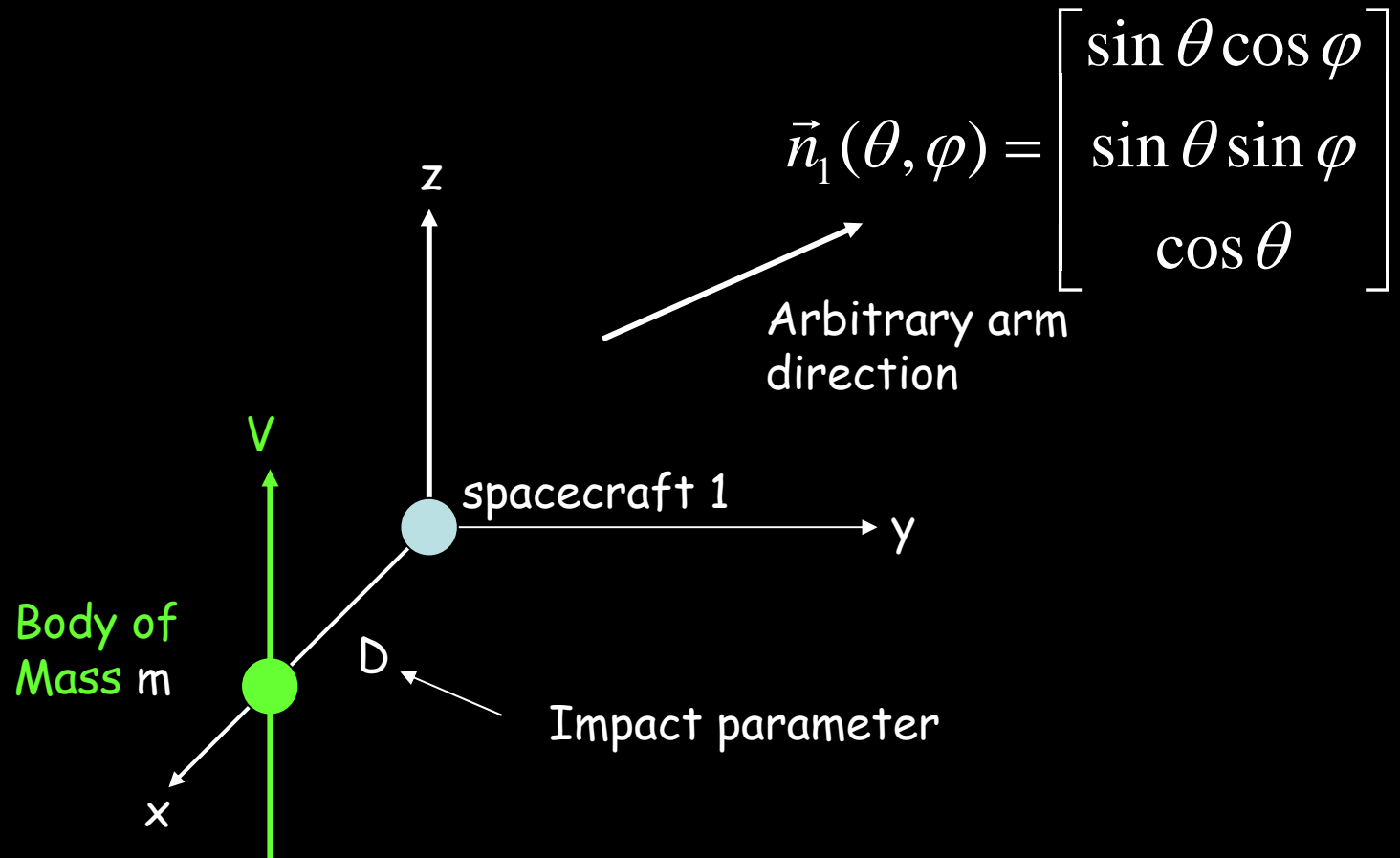


LISA response

Combinaisons TDI (X, α, ζ) :

$$X = V_1 + U_1 = 2(\vec{n}_2 + \vec{n}_3) \cdot \frac{\vec{v}}{c} = -2\vec{n}_1 \cdot \frac{\vec{v}}{c}$$

natural frame



Motion of spacecraft

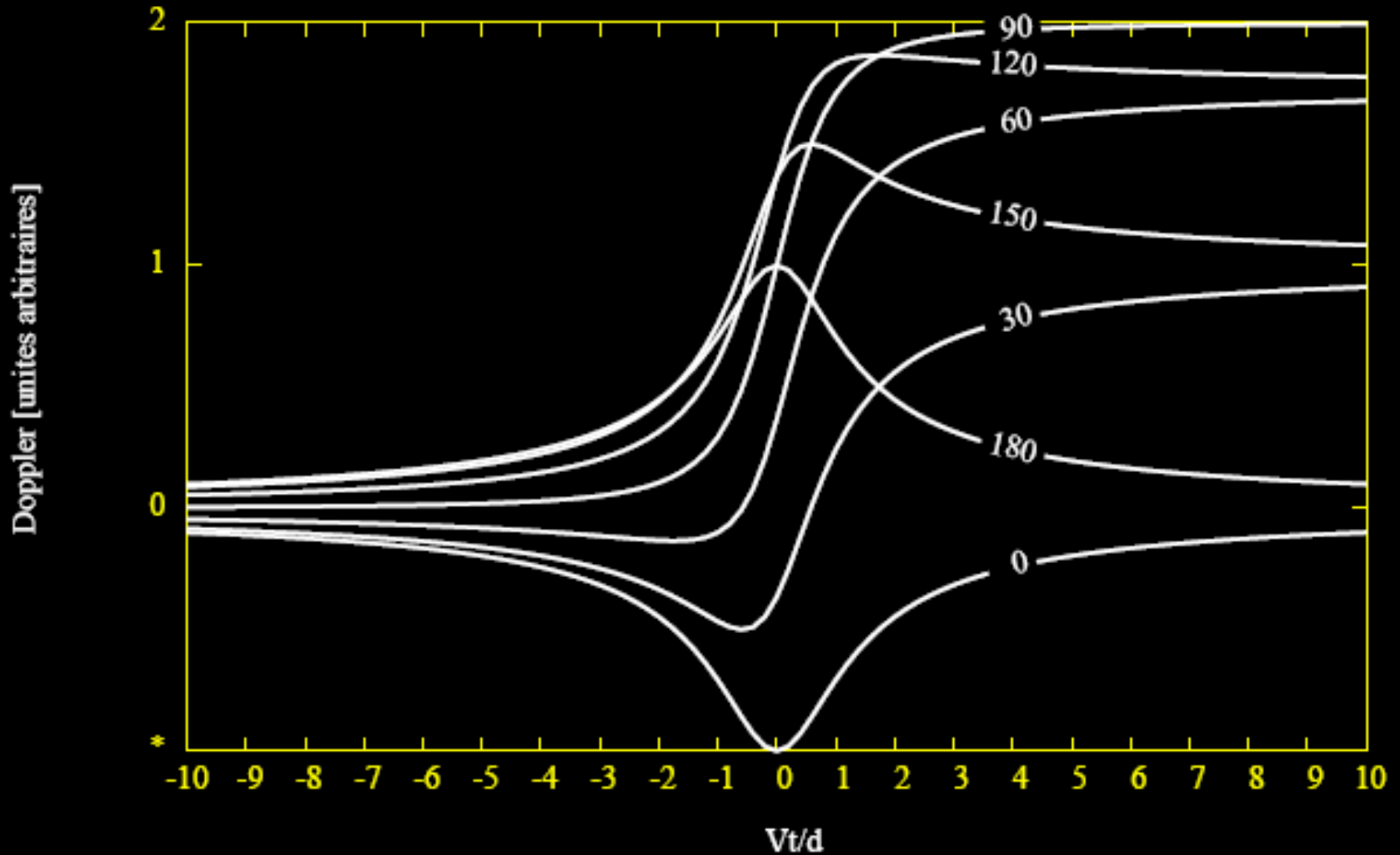
$$\vec{\Gamma}(t) = \frac{Gm}{D^2} \frac{1}{\left(1 + V^2 t^2 / D^2\right)^{3/2}} \begin{bmatrix} 1 \\ 0 \\ Vt / D \end{bmatrix}$$

$$\vec{v}(t) = \frac{Gm}{DV} \begin{bmatrix} 1 + \frac{Vt / D}{\left(1 + V^2 t^2 / D^2\right)^{1/2}} \\ 0 \\ -\frac{1}{\left(1 + V^2 t^2 / D^2\right)^{1/2}} \end{bmatrix}$$

Response filtered by TDI

$$X(t) = -\frac{2Gm}{DVc} \left\{ \sin \theta \cos \varphi \left(1 + \frac{Vt/D}{\sqrt{1+V^2t^2/D^2}} \right) - \cos \theta \frac{1}{\sqrt{1+V^2t^2/D^2}} \right\}$$

$X(t)$ for various orientations (degrees) θ ($\varphi = 0$)



Fourier space

$$\tilde{\vec{\Gamma}}(\omega) = \frac{2Gm\omega}{V^2} \begin{bmatrix} K_1(\omega D/V) \\ 0 \\ -iK_0(\omega D/V) \end{bmatrix}$$

$$\frac{\tilde{\vec{v}}}{c}(\omega) = \frac{2Gm}{cV^2} \begin{bmatrix} iK_1(\omega D/V) \\ 0 \\ K_0(\omega D/V) \end{bmatrix}$$

*(K_n : 2d kind
modified Bessel f.)*

$$\tilde{X}(\omega) = -\frac{4Gm}{cV^2} \left[iK_1(\omega D/V) \sin \theta \cos \varphi + K_0(\omega D/V) \cos \theta \right]$$

Spectral density of noise and SNR

$$S_X(f) = \left[8 \sin^2(4\pi fL/c) + 32 \sin^2(2\pi fL/c) \right] S_{acc}(f) + 16 \sin^2(2\pi fL/c) S_{bq}(f)$$

Acceleration noise

Optical path noise

Angular average:

$$\left\langle \left| \tilde{X}(f) \right|^2 \right\rangle = \frac{1}{3} \left(\frac{4Gm}{cV^2} \right)^2 \left[K_1^2(2\pi fD/V) + K_0^2(2\pi fD/V) \right]$$

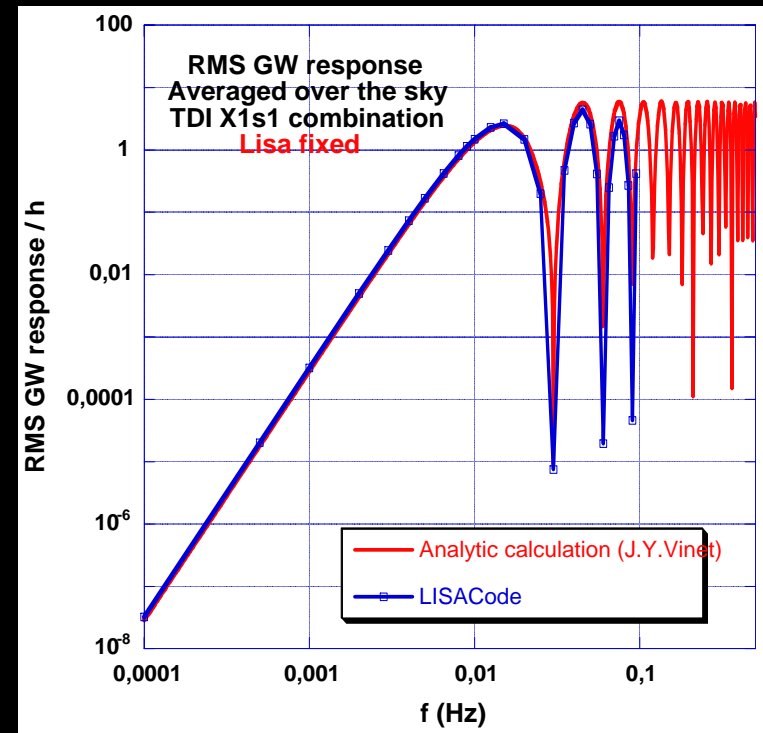
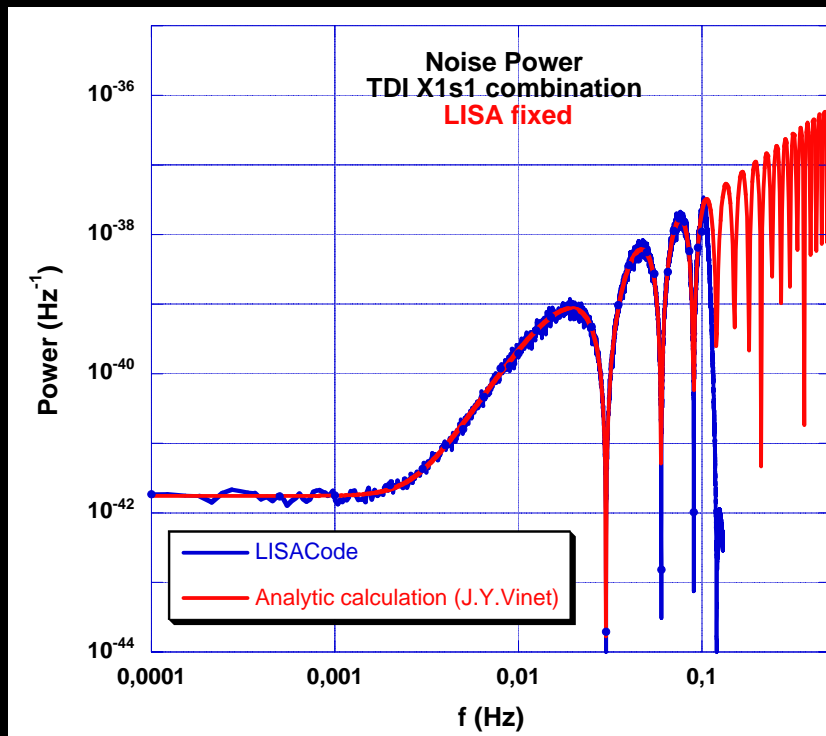
SNR power
Spectral density

$$\rho(f) = 4 \frac{\left\langle \left| \tilde{X}(f) \right|^2 \right\rangle}{S_X(f)}$$

Linear Spectral Density Of residual noise

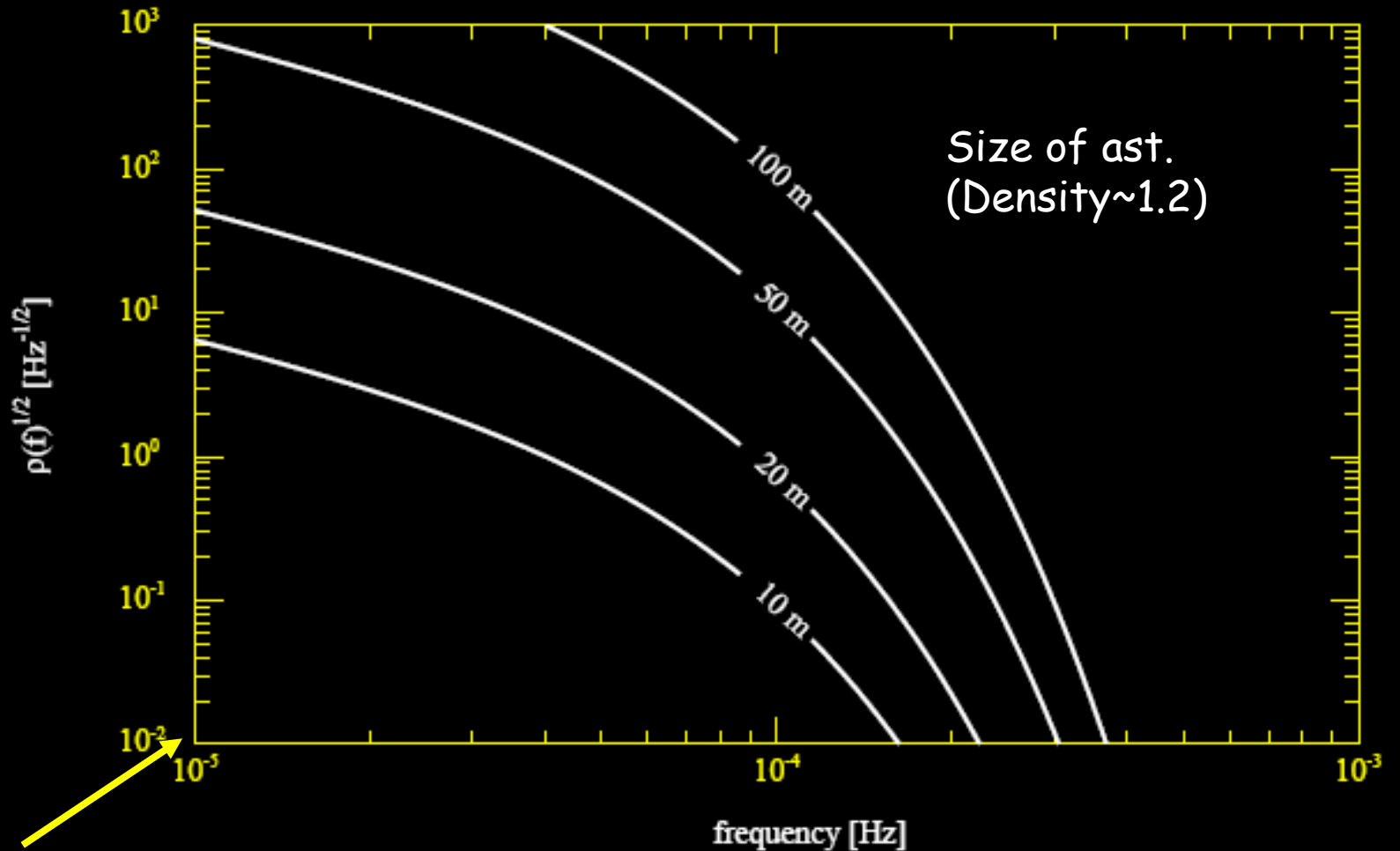
$$S_X^{1/2}(f)$$

Response to GW signal



Linear spectral density of SNR for $V=20$ km/s

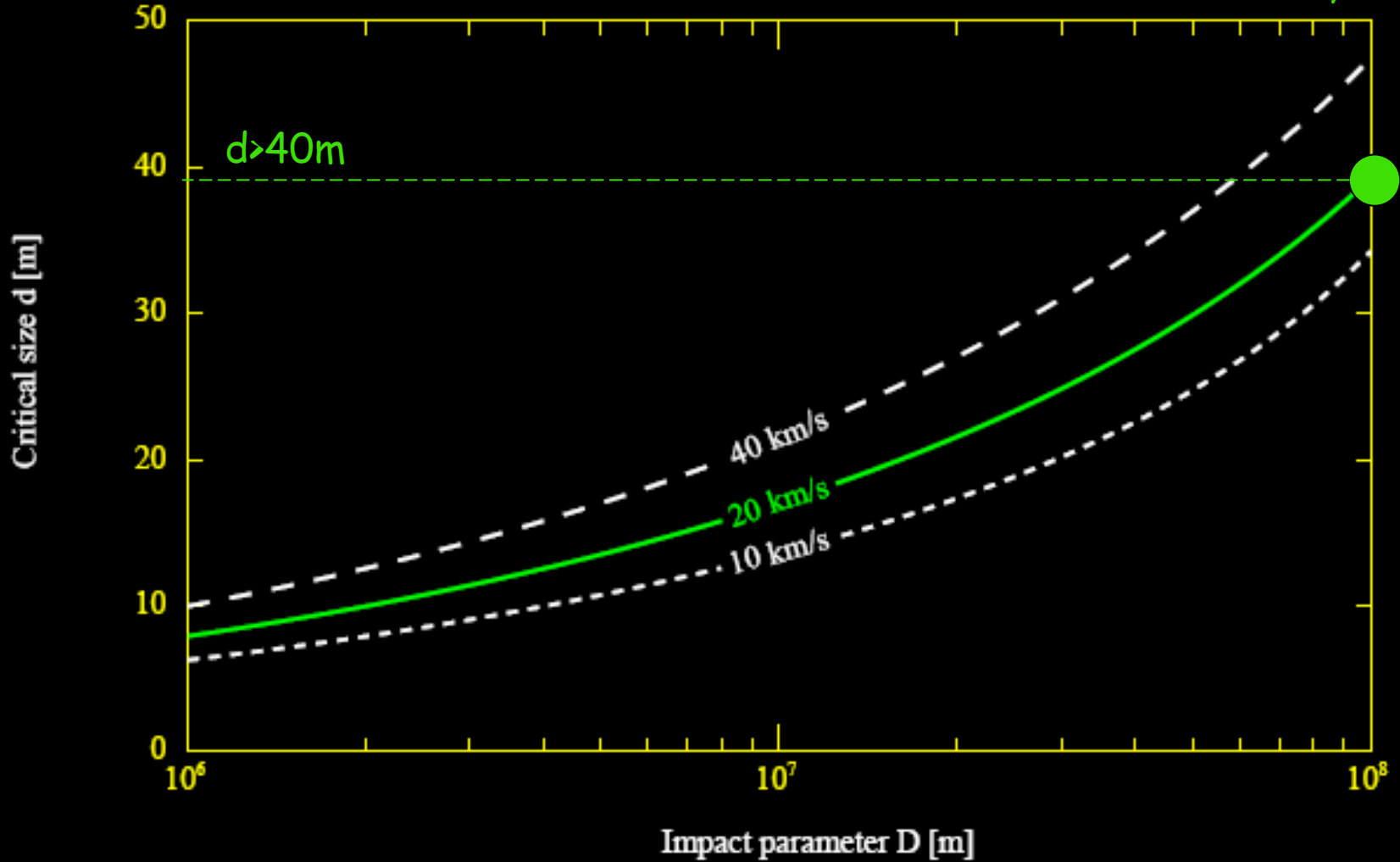
Impact parameter : 100,000 km



Cutoff frequency

Detection condition (SNR>1)

D=100,000km



Programme:

Assesment of a rate of detection

Monte Carlo simulation using
Realistic distributions of
asteroids masses and velocities